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# Microwave dielectric properties of a low firing and temperature stable lithium magnesium tungstate ( $\text{Li}_4\text{MgWO}_6$ ) ceramic with a rock-salt variant structure

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## ABSTRACT

The  $\text{Li}_4\text{MgWO}_6$  ceramic was synthesized by the conventional solid-state reaction method, and its sintering behavior and microwave dielectric properties were studied for the first time. The XRD patterns and structural refinements indicated that  $\text{Li}_4\text{MgWO}_6$  formed an orthorhombic phase at temperatures above 900 °C, and TEM analyses confirmed the ordered and layered rock-salt superstructures for the orthorhombic  $\text{Li}_4\text{MgWO}_6$ . The SEM photographs and relative density curve showed that the sample sintered at 950 °C had the highest densification. When sintered at 950 °C in a  $\text{WO}_3$ -rich atmosphere for 4 h,  $\text{Li}_4\text{MgWO}_6$  had the following optimum properties:  $\epsilon_r = 15.06 \pm 0.33$ ,  $Q \times f = 28,300 \pm 600$  GHz ( $f = 10.1$  GHz), and  $\tau_f = 0.9 \pm 3.4$  ppm/°C. Compared with other reported low permittivity compounds,  $\text{Li}_4\text{MgWO}_6$  shows more potential for the Low-Temperature Cofired Ceramics (LTCC) substrate materials due to its intrinsic low sintering temperature, novel temperature stability, and relatively low dielectric loss.

## 1. Introduction

Low dielectric permittivity plays a vital role in the propagation of high-velocity signals through a dielectric medium, and dielectric materials with low permittivities ( $\epsilon_r$ , generally less than 20) are frequently used as substrate materials for millimeter-wave applications [1–3]. The low-temperature co-fired ceramic (LTCC) technology is one of the most important methods for integrating chip components on dielectric substrates [4]. The materials for LTCC applications should have sintering temperatures lower than the melting point of the co-fired electrodes, of which the most commonly used electrode is silver with a melting point of 961 °C. Unfortunately, numerous promising substrate candidates,

such as  $\text{Mg}_2\text{SiO}_4$  (1450 °C) [5],  $\text{ZnAl}_2\text{O}_4$  (1375 °C) [6],  $\text{CaMgSi}_2\text{O}_6$  (1300 °C) [7],  $\text{Li}_3\text{Mg}_2\text{NbO}_6$  (1250 °C) [8],  $\text{Li}_2\text{TiO}_3$  (1230 °C) [9], and  $\text{Li}_3\text{NbO}_4$  (1150 °C) [8] possess relatively high sintering temperatures. Recent efforts have focused on modifying the dielectric properties of rock-salt structured  $\text{Li}_3\text{Mg}_2\text{NbO}_6$ ,  $\text{Li}_2\text{TiO}_3$ , and  $\text{Li}_3\text{NbO}_4$ -based ceramics for LTCC applications as these lithium-containing ceramics have lower sintering temperatures near the LTCC requirement [10–12]. In these ceramics, stability over a wide range of temperatures is vital for practical applications of LTCC materials, but most of the low permittivity matrix ceramics possess negative temperature coefficients of the resonant frequency ( $\tau_f$ ) [13]; only a few exhibited positive  $\tau_f$  values, such as  $\text{Li}_2\text{SnO}_3$  ( $\epsilon_r = 12.8$ ,  $Q \times f = 20,800$  GHz,  $\tau_f = 26.9$  ppm/°C) [9],  $\text{Li}_2\text{TiO}_3$  ( $\epsilon_r =$

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19.8,  $Q \times f = 23,600$  GHz,  $\tau_f = 38.5$  ppm/ $^{\circ}$ C [9],  $\text{NiCu}_2\text{Nb}_2\text{O}_8$  ( $\epsilon_r = 12.8$ ,  $Q \times f = 4200$  GHz,  $\tau_f = 481.6$  ppm/ $^{\circ}$ C [14], and  $\text{LaNbO}_4$  ( $\epsilon_r = 19.3$ ,  $Q \times f = 54,400$  GHz,  $\tau_f = 9.0$  ppm/ $^{\circ}$ C [15], and it is rare that a low-permittivity compound has a near-zero  $\tau_f$  value. While a near-zero  $\tau_f$  can be achieved by compositing two phases with opposite  $\tau_f$  values, other properties would be influenced. Similarly, while the sintering temperature could be reduced by introducing a glassy phase into the ceramic material, such a change would likely alter the dielectric permittivity and thermal stability as well as deteriorate the  $Q \times f$  values [16]. Therefore, it would be complex to develop a new glass-ceramic composite to satisfy the needs of LTCC applications. It frequently requires trial-and-error tests to find both an appropriate glass additive and a dopant phase with an opposite  $\tau_f$  to the matrix to modify both the sintering temperature and temperature stability in the meantime. However, luckily, glass-free ceramics with intrinsically low sintering temperatures were more beneficial for performance modification, saving time and cost for the formula research and production of complex glass additives. Numerous recently developed glass-free ceramics concerning Bi, Mo, V, and W-based compounds, are well-suited for LTCC applications [17–19].

Specifically, lithium tungsten oxide glass-free microwave dielectric ceramics have received much attention due to their excellent dielectric performance. For example,  $\text{Li}_4\text{WO}_5$  has a pure rock-salt phase and novel temperature-stable properties as  $\epsilon_r = 8.6$ ,  $Q \times f = 23,100$  GHz, and  $\tau_f = -2.6$  ppm/ $^{\circ}$ C when sintered at  $890^{\circ}\text{C}$  for 2 h [20]. The phenacite  $\text{Li}_2\text{WO}_4$  ceramic has a quite low intrinsic sintering temperature, and it showed good properties of  $\epsilon_r = 5.5$ ,  $Q \times f = 62,000$  GHz, and  $\tau_f = -146$  ppm/ $^{\circ}$ C when sintered at  $650^{\circ}\text{C}$  for 2 h [21]. Also, the lithium magnesium tungstate ceramics, chemically formulated as  $\text{Li}_2\text{Mg}_2\text{W}_2\text{O}_9$  and  $\text{Li}_2\text{Mg}_2(\text{WO}_4)_3$ , showed good dielectric performance. The former showed the properties of  $\epsilon_r = 11.5$ ,  $Q \times f = 31,900$  GHz, and  $\tau_f = -66$  ppm/ $^{\circ}$ C when well-sintered at  $920^{\circ}\text{C}$  for 4 h, and the latter showed the properties of  $\epsilon_r = 8.2$ ,  $Q \times f = 90,000$  GHz, and  $\tau_f = -52.4$  ppm/ $^{\circ}$ C when sintered at  $900^{\circ}\text{C}$  for 4 h [22,23]. Generally, the abovementioned compounds can be indexed to the  $\text{Li}_2\text{O}$ - $\text{WO}_3$ - $\text{MgO}$  ternary phase diagram, as plotted in Fig. 1, wherein the  $\text{Li}_2\text{W}_2\text{O}_7$  [24] and  $\text{MgWO}_4$  [25] compounds with good microwave dielectric properties were also added.

There is a largely unexploited area in the  $\text{Li}_2\text{O}$ -rich part of the ternary phase diagram (Fig. 1). We have noticed that while  $\text{Li}_4\text{MgWO}_6$ , a single monoclinic rock salt structure when calcined at  $600^{\circ}\text{C}$ , was first synthesized by Mandal et al. as a precursor to prepare  $\text{Sr}_2\text{MgWO}_6$  ceramics [26], no further work has been conducted on the functional properties of  $\text{Li}_4\text{MgWO}_6$  to date. In this work,  $\text{Li}_4\text{MgWO}_6$  ceramic was synthesized, and its crystal structure, sintering behavior, and microwave dielectric properties were studied.

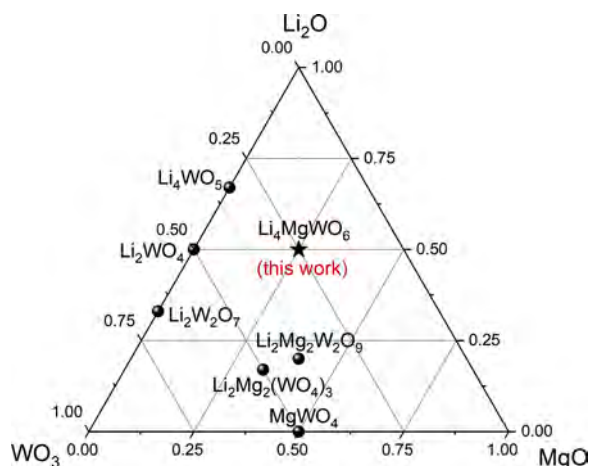


Fig. 1. Phase diagrams of the  $\text{Li}_2\text{O}$ - $\text{WO}_3$ - $\text{MgO}$  ternary system.

## 2. Materials and methods

Ceramic  $\text{Li}_4\text{MgWO}_6$  was synthesized by the conventional solid-state reaction method. All the reactants, the  $\text{Mg}(\text{OH})_2 \cdot 4\text{MgCO}_3 \cdot 5\text{H}_2\text{O}$  (99.00 %),  $\text{Li}_2\text{CO}_3$  (99.90 %), and  $\text{WO}_3$  (99.90 %), were mixed by ball milling for 8 h in a nylon jar using zirconia balls and ethyl alcohol as the media. The slurries were dried for 6 h and then calcined at  $750^{\circ}\text{C}$  for 4 h. The powders were then reground using the same method as above for 3 h. After drying, the resulting powders were granulated by adding an 8% polyvinyl alcohol (PVA) in an agate mortar. They were shaped into cylinders of diameter 12 mm and length 6 mm under a pressure of 22 MPa. Tungsten trioxide has a sublimation temperature of about  $900^{\circ}\text{C}$  [27]. To prevent the  $\text{WO}_3$  from subliming at the sintering temperature range, we put the samples on an  $\text{Al}_2\text{O}_3$  groove with an  $\text{Al}_2\text{O}_3$  crucible covered, and the interface between the crucible and the groove was buried with sufficient  $\text{WO}_3$  powder, in which the sacrificial  $\text{WO}_3$  powder provided a  $\text{WO}_3$ -rich atmosphere during the sintering. Then a giant  $\text{Al}_2\text{O}_3$  crucible covered this whole set to preserve the  $\text{WO}_3$ -rich atmosphere. In this way, the samples were sintered in a controlled  $\text{WO}_3$ -rich atmosphere from  $910^{\circ}\text{C}$  to  $990^{\circ}\text{C}$  for 4 h.

The bulk densities were measured by the Archimedes' method, and the relative densities were calculated as the ratios of the observed densities to the theoretical densities. The X-ray powder diffraction patterns were scanned in  $2\theta$  ranges from  $13^{\circ}$  to  $90^{\circ}$  with a step size of  $0.0131^{\circ}$ , measured on a laboratory X-ray diffractometer (Philips X'Pert Pro MPD, Netherlands). The Rietveld method was conducted using the General Structure Analysis System (GSAS) coupled with the EXPGUI program to perform structure refinement [28,29]. The TG-DSC (thermogravimetric-differential scanning calorimeter) signals were obtained using a simultaneous thermal analysis (Netzsch STA 449C, Germany) with a heating rate of  $10^{\circ}\text{C}/\text{min}$  in dry air. The shrinkage curves of the samples were measured on a horizontal loading dilatometer (Netzsch, Germany). The polished and thermally etched surface morphologies were observed by scanning electron microscopy (SEM, FEI Inspect F, England). Before SEM observations, the ceramic samples were polished on abrasive paper (1200 mesh) and thermally etched at temperatures of  $30^{\circ}\text{C}$  below the sintering temperatures for 30 min. High-resolution transmission electron microscopy (HR-TEM) images and selected area electron diffractions (SAEDs) were obtained on a TEM microscope (Tecnai G2 F20 S-Twin TMP, USA) operated at 200 kV. Microwave dielectric properties were measured by a network analyzer (Agilent Technologies E5071C, USA) using the Hakki-Coleman method in TE011 mode [30]. The temperature coefficients of the resonant frequency ( $\tau_f$ ) were measured by the network analyzer coupled with a temperature chamber (DELTA 9023, Delta Design, USA), and calculated using the relation:

$$\tau_f = \frac{f_2 - f_1}{f_1(t_2 - t_1)} \quad (1)$$

where  $f_1$  and  $f_2$  represent the resonant frequencies at  $t_1 = 25^{\circ}\text{C}$  and  $t_2 = 85^{\circ}\text{C}$ , respectively. Dielectric permittivity variation in the temperature range of  $-55$  to  $125^{\circ}\text{C}$  was measured under 1 MHz frequency by a precision LCR meter (Agilent 4284A, USA) and an automatic temperature controller. The temperature coefficient of permittivity ( $\tau_\epsilon$ ) was obtained by:

$$\tau_\epsilon = \frac{\epsilon_2 - \epsilon_1}{\epsilon_1(t_2 - t_1)} \quad (2)$$

where  $\epsilon_1$  is the permittivity at  $t_1 = 25^{\circ}\text{C}$  and  $\epsilon_2$  is the permittivity within  $25^{\circ}\text{C} < t_2 \leq 125^{\circ}\text{C}$ . The thermal expansion coefficient ( $\alpha_L$ ) was measured by a thermo-mechanical analysis (TMA, Netzsch DIL 420C, Germany).

### 3. Results and discussions

Fig. 2 shows the XRD patterns of the  $\text{Li}_4\text{MgWO}_6$  ceramics sintered at temperatures ranging from 910 to 990 °C for 4 h. The patterns can be indexed to the orthorhombic structure according to the profile of the  $\text{Li}_3\text{Mg}_2\text{NbO}_6$  (JCPDS no. 86-0346) phase with the space group  $Fddd$  (70). Impure peaks, at around  $2\theta = 18.8^\circ$  and  $21.0^\circ$ , with low intensities indicated a tiny amount secondary phase was formed in the samples sintered above 900 °C. Based on the XRD data of the raw powders (Fig. S1), there is a monoclinic–orthorhombic phase transition driven by the temperature change from 800 °C to 900 °C. According to the peak profile of the monoclinic phase, the secondary phase might be the unreacted monoclinic  $\text{Li}_4\text{MgWO}_6$  phase, which can be indexed according to the model of  $\text{Li}_5\text{ReO}_6$  (JCPDS no. 82-0929) in the  $C2/m$  (12) space group. However, the Rietveld refinement results indicated that the weight fractions of the monoclinic secondary phase were relatively small ( $\text{wt.}\% = 1\text{--}2\%$ ) when the sintering temperature exceeded 930 °C, as shown in Fig. 2 (c). Hence, the effects of the monoclinic phase on the structural and dielectric properties can be negligible. For more information on the reactions of the raw powders, see Eqs. S1–S8. Similarly, a cubic–orthorhombic phase transition has been reported for  $\text{Li}_4\text{WO}_5$  ceramic in the temperature range from 680 °C to 750 °C [20]. These temperature-driven phase transitions for tungstate may be ascribed to the structure variation of tungsten trioxide with the temperature change.  $\text{WO}_3$  is tetragonal at temperatures above 740 °C and is orthorhombic from 330 to 740 °C [31].

The Rietveld refinement profile of the  $\text{Li}_4\text{MgWO}_6$  ceramic sintered at 950 °C is shown in Fig. 3 (a), and the insert image exhibits the schematic of the crystal structure for the orthorhombic phase. The orthorhombic  $\text{Li}_4\text{MgWO}_6$  phase has a crystal symmetry in an ordered rock-salt type, namely the  $Fddd$  space group. In this structure, the cations and anions are octahedrally coordinated by each other, similar to that of the  $\text{Li}_3\text{Mg}_2\text{NbO}_6$  prototype [32]. The SAED pattern (Fig. 3 (b)) for the orthorhombic  $\text{Li}_4\text{MgWO}_6$  ceramic exhibits superlattice reflections arising from the cation ordering, which may be ascribed to the Li/Mg ordered arrangement over a superstructure period. The HR-TEM image (Fig. 3 (c)) confirmed the ordered and layered structure for the orthorhombic  $\text{Li}_4\text{MgWO}_6$  phase. The corresponding structural characteristics for the monoclinic  $\text{Li}_4\text{MgWO}_6$  ceramic calcined at 750 °C are shown in Fig. S2. The monoclinic phase has a rock-salt superstructure as well but a different site symmetry ( $C2/m$ ). The detailed crystallographic data derived from the refinement results for both structures are shown in

Table S1.

Fig. 4 shows the TG-DSC results for the  $\text{Li}_4\text{MgWO}_6$  raw powder and linear shrinkage curve of the  $\text{Li}_4\text{MgWO}_6$  ceramic as a function of temperature. The mass loss stages at temperatures below 700 °C were attributed to the decomposition of raw powder (dehydration and carbonate decomposition), and the slight mass loss at temperatures above 709 °C may be ascribed to the  $\text{WO}_3$  sublimation in air [27]. According to the phase types of raw powders in the wide temperature range (Fig. S1), the endothermic peak located at 626 °C was related to the generation of the monoclinic phase, and two of the intense peaks ranging from 700 to 800 °C corresponded to the phase transition process from the monoclinic to the orthorhombic and the formation of the orthorhombic  $\text{Li}_4\text{MgWO}_6$  phase, respectively. The shrinkage curve indicated that the densification process started at around 820 °C, the temperature near the formation period of the orthorhombic  $\text{Li}_4\text{MgWO}_6$  phase, and the fastest contraction rate was at about 925 °C.

SEM images of the polished and thermally etched surfaces of the  $\text{Li}_4\text{MgWO}_6$  samples sintered at the temperature range from 910 to 990 °C for 4 h were shown in Fig. 5 (a–e), and the insert graphs show the grain size distributions and the average grain sizes. The grains were small, and numerous micropores were observed in the sample sintered at 910 °C, which indicated insufficient sintering. Neat and uniform grains were observed for the samples sintered at 930 °C and 950 °C, and no apparent micropores were detected in these well-sintered samples. The grain boundaries appeared to melt in the sample sintered at 970 °C. As the sintering temperature increased further to 990 °C, the grain boundaries of the sample melted more severely, and pores became larger, indicated oversintering. The average grain size increased continuously with the rising temperature. The morphologies of the cross-sections and surfaces of the as-sintered samples are shown in Fig. S3 and Fig. S4, respectively. Both the surface and cross-section morphologies showed that the sample sintered at 950 °C had the most highly densified microstructures. Compared Fig. 5 with Fig. S4, it can be seen the pores were further eliminated after the polishing and thermally etching.

The relative density ( $\rho_{\text{re}}$ ) of the  $\text{Li}_4\text{MgWO}_6$  ceramics as a function of the sintering temperature is shown in Fig. 6 (a). With the increasing temperature, the  $\rho_{\text{re}}$  first increased, peaked at 95.66 % (theoretical density was  $5.08 \text{ g/cm}^3$ ) at 950 °C and then decreased. The porosity ( $P = 1 - \rho_{\text{re}}$ ) variation followed the changing trend of the number of pores in the microstructures, as indicated in Fig. 5. The optimum relative density of the samples was higher than that of a few typical Li-containing

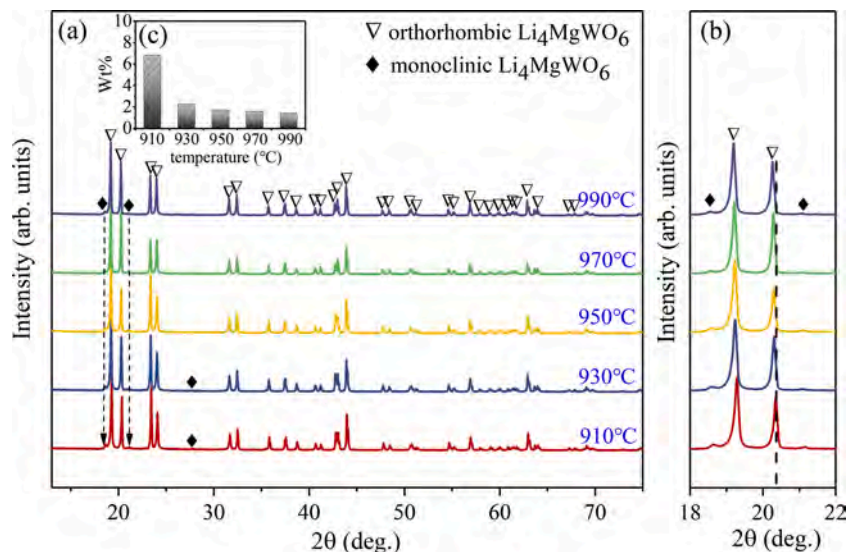
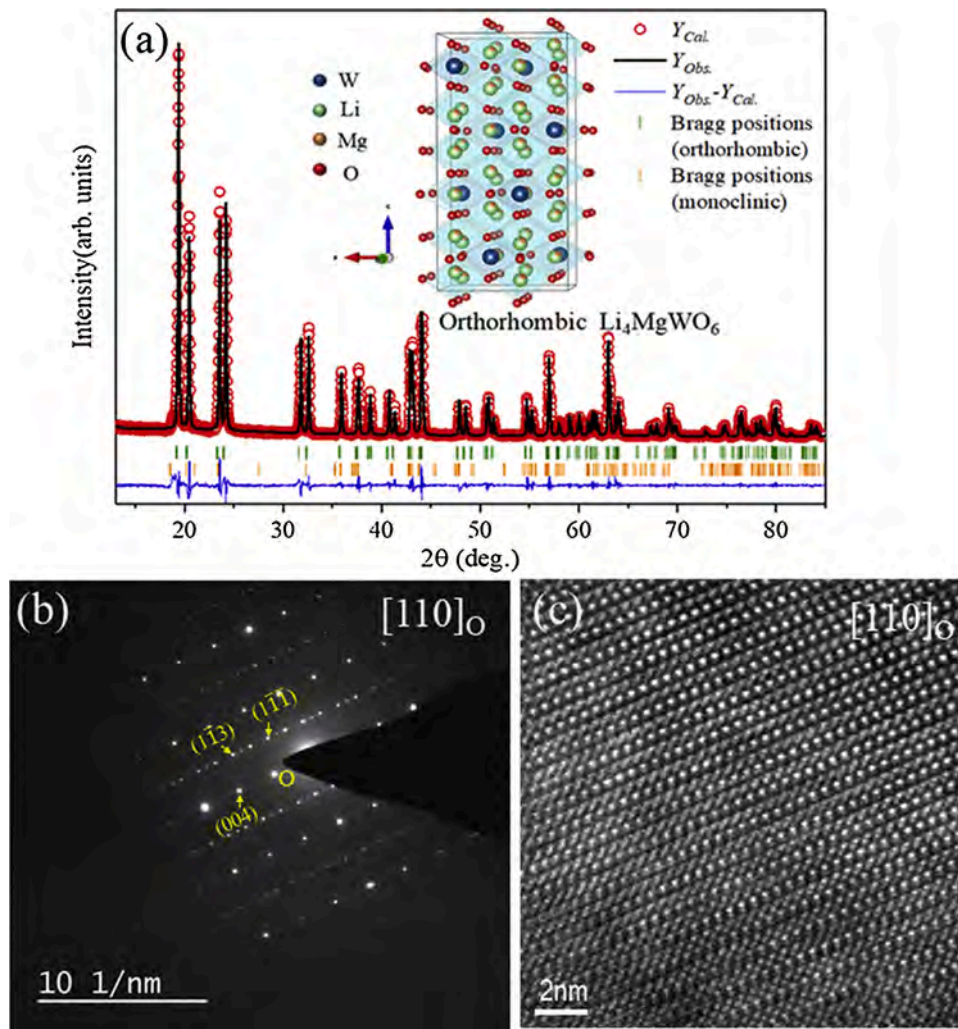
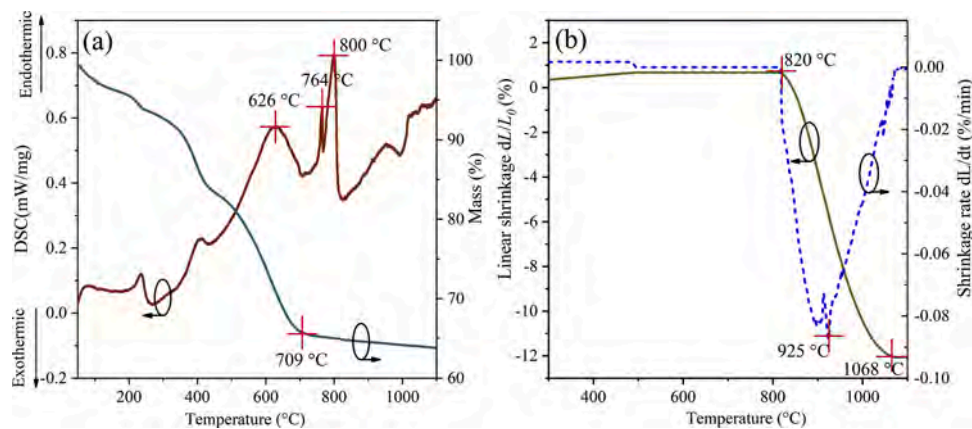


Fig. 2. (a) XRD patterns of the  $\text{Li}_4\text{MgWO}_6$  ceramics sintered at 910 – 990 °C for 4 h. (b) Enlarged image of the XRD patterns ranges from 18 to 22 degrees. (c) Weight fractions ( $\text{wt.}\%$ ) of the monoclinic secondary phase.





**Fig. 3.** (a) Rietveld refinement profile of  $\text{Li}_4\text{MgWO}_6$  ceramic sintered at 950 °C for 4 h, the insert image was the schematic of the orthorhombic crystal structure for  $\text{Li}_4\text{MgWO}_6$ . (b) SAED pattern of the orthorhombic  $\text{Li}_4\text{MgWO}_6$  taken along [110] zone axis and (c) the corresponding HR-TEM image.

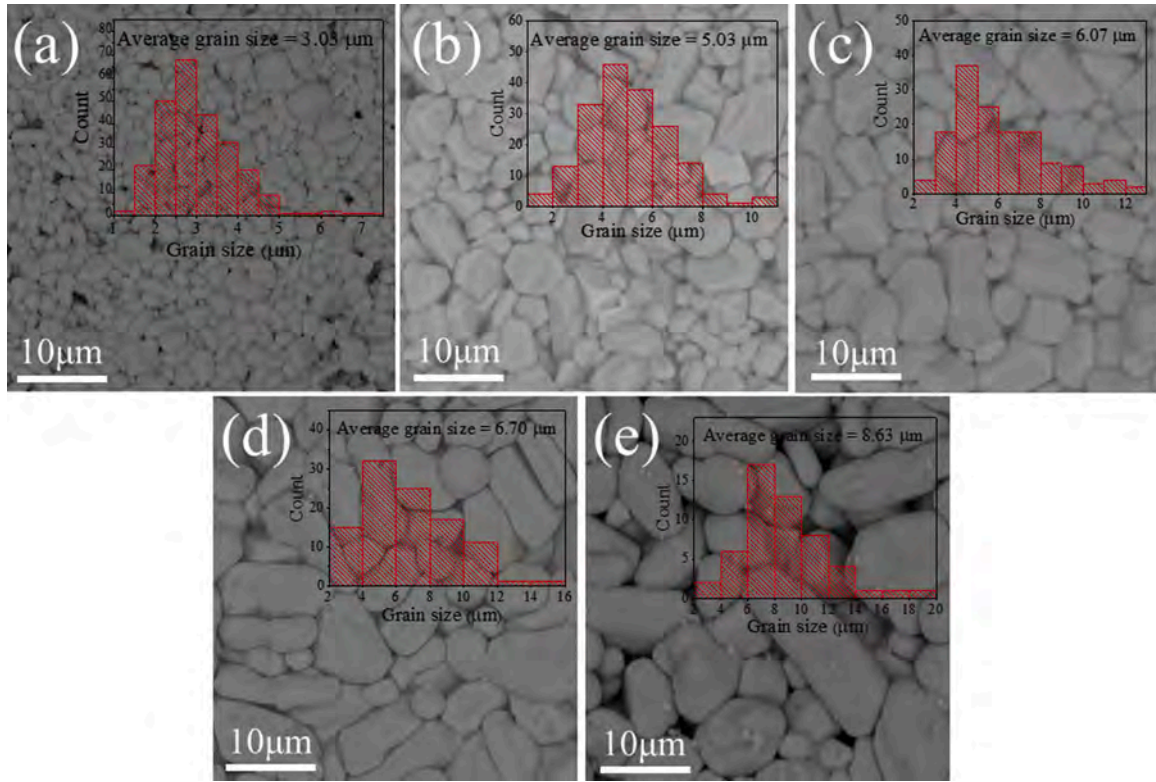


**Fig. 4.** (a) TG-DSC of the  $\text{Li}_4\text{MgWO}_6$  raw powder and (b) linear shrinkage and shrinkage rate curves of the  $\text{Li}_4\text{MgWO}_6$  ceramic.

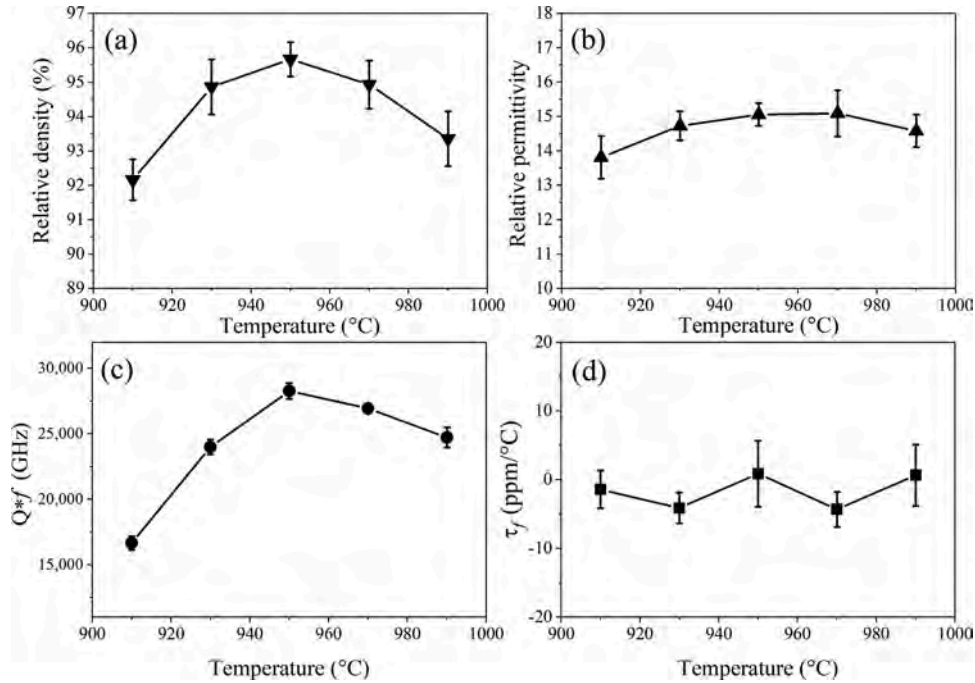
ceramics sintered at relatively higher temperatures, such as  $\text{Li}_2\text{TiO}_3$  ( $\rho_{\text{re}} \sim 93\%$ , 1300 °C) [33],  $\text{Li}_2\text{Mg}_3\text{TiO}_6$  ( $\rho_{\text{re}} \sim 94\%$ , 1360 °C) [34], and  $\text{Li}_2\text{MgTiO}_4$  ( $\rho_{\text{re}} \sim 91\%$ , 1360 °C) [35]. These ceramics showed highly porous microstructures because of the lithia evaporation at above 1000 °C [36]. It is reasonable that, to some extent, the high density was attained because the  $\text{Li}_4\text{MgWO}_6$  sample can be densified below the

evaporating point of lithium oxide. Similar degrees of high densifications were also achieved in two other lithium magnesium tungstate ceramics of  $\text{Li}_2\text{Mg}_2\text{W}_2\text{O}$  ( $\rho_{\text{re}} \sim 95\%$ , 920 °C) [22] and  $\text{Li}_2\text{Mg}_2(\text{WO}_4)_3$  ( $\rho_{\text{re}} \sim 96\%$ , 800 °C) [23] that were sintered below 1000 °C.

The relative permittivity ( $\epsilon_r$ ) showed a similar variation to the relative density with the increasing temperature, as plotted in Fig. 6 (b). The



**Fig. 5.** SEM micrographs of the polished and thermally etched surface of the  $\text{Li}_4\text{MgWO}_6$  ceramics sintered at (a) 910 °C, (b) 930 °C, (c) 950 °C, (d) 970 °C, and (e) 990 °C for 4 h. The insert graphs show the grain size distributions and the average grain sizes.



**Fig. 6.** (a) Relative density ( $\rho_r$ ), (b) relative permittivity ( $\epsilon_r$ ), (c)  $Q \times f$  value, and (d) temperature coefficient of the resonant frequency ( $\tau_f$ ) of the  $\text{Li}_4\text{MgWO}_6$  ceramics as a function of temperature.

low relative permittivity of  $\text{Li}_4\text{MgWO}_6$  can be attributed to the low ion dielectric polarizabilities of  $\text{Li}^+$  ( $\alpha = 1.20 \text{ \AA}^3$ ) and  $\text{Mg}^{2+}$  ( $\alpha = 1.32 \text{ \AA}^3$ ) and moderate ionic polarizability of  $\text{W}^{6+}$  ( $\alpha = 3.20 \text{ \AA}^3$ ) ions [37]. The magnitude of the theoretical relative permittivity contributed by the ionic polarizabilities for a known structure can be estimated by the

Clausius-Mosotti equation [37]:

$$\epsilon_{r(\text{theo})} = \frac{3V_m + 8\pi\alpha_D}{3V_m - 4\pi\alpha_D} \quad (3)$$

where  $V_m$  is the volume of the unit cell, and  $\alpha_D$  is the total molecular

polarizability. The  $\alpha_D$  of  $\text{Li}_4\text{MgWO}_6$  can be calculated by the following relationship:

$$\alpha_D(\text{Li}_4\text{MgWO}_6) = 4\alpha(\text{Li}^+) + \alpha(\text{Mg}^{2+}) + \alpha(\text{W}^{6+}) + 6\alpha(\text{O}^{2-}) \quad (4)$$

The  $\varepsilon_{r(\text{theo})}$  was calculated as 15.22 for the sample sintered at 950 °C, close to the observed  $\varepsilon_r$  value of 15.06, indicating that there were not many "rattling" or "compressed" cations and dipolar impurities that could lead to permittivity deviation in the  $\text{Li}_4\text{MgWO}_6$  ceramic [37].

The  $Q \times f$  values highly depend on porosity, and the variation of the  $Q \times f$  values corresponded closely to the changing trend of the relative density, as shown in Fig. 6(c). However, for well-dense structures ( $\rho_{\text{re}} > 95\%$ ), the packing fraction plays a more crucial role in the dielectric loss [38]. The packing fraction (P.F) was defined as [38]:

$$\text{Packing fraction} = \frac{\text{volume of the atoms in the cell}}{\text{volume of the unit cell}} \times Z \quad (5)$$

where  $Z$  is 8 for the  $\text{Li}_4\text{MgWO}_6$  ceramic. The packing fraction of the  $\text{Li}_4\text{MgWO}_6$  ceramic sintered at 950 °C was calculated as 72.7 %, which was similar to the typical ceramics with the close packing rock-salt structures, such as  $\text{Li}_3\text{Mg}_2\text{NbO}_6$  (P.F ~ 70.0 %) [39],  $\text{Li}_2\text{MgTiO}_4$  (P.F ~ 75.1 %) [40], and  $\text{Li}_2\text{TiO}_3$  (P.F ~ 73.0 %) [41]. Because of the highly packed crystal structures, all these ceramics showed relatively low dielectric losses.

The temperature coefficients of the resonant frequency ( $\tau_f$ ) are displayed in Fig. 6 (d). In the sintering temperature range, the measured  $\tau_f$  values are within the scope from -6.0 to +4.3 ppm/°C. The  $\tau_f$  value has a relation with the temperature coefficient of the relative permittivity ( $\tau_\varepsilon$ ) as follows [42]:

$$\tau_f = -(\alpha_L + \frac{\tau_\varepsilon}{2}) \quad (6)$$

where  $\alpha_L$  is the thermal expansion coefficient. Fig. 7 (a) shows the relative permittivity as a function of temperature (-55 – 125 °C) at 1 MHz frequency. The insert image of Fig. 7 (a) shows the  $\tau_\varepsilon$  values in a wide temperature range ( $t_2 = 30$ –125 °C,  $t_1 = 25$  °C), and the  $\tau_\varepsilon$  value between 25 °C and 85 °C was -10.1 ppm/°C. The sample has a linear thermal expansion, and  $\alpha_L$  has a relatively large value of +13.2 ppm/°C between 25 °C and 85 °C, as shown in Fig. 7 (b). Thus, the  $\tau_f$  value can be calculated by Eq. 6, the result value was -8.15 ppm/°C and not far from the measure ones ( $0.9 \pm 3.4$  ppm/°C). This deviation can be ascribed to the different measured frequencies, and a similar phenomenon was reported in other literature [43]. According to Bosman and Havinga's expression, three effects contribute to the temperature dependence of

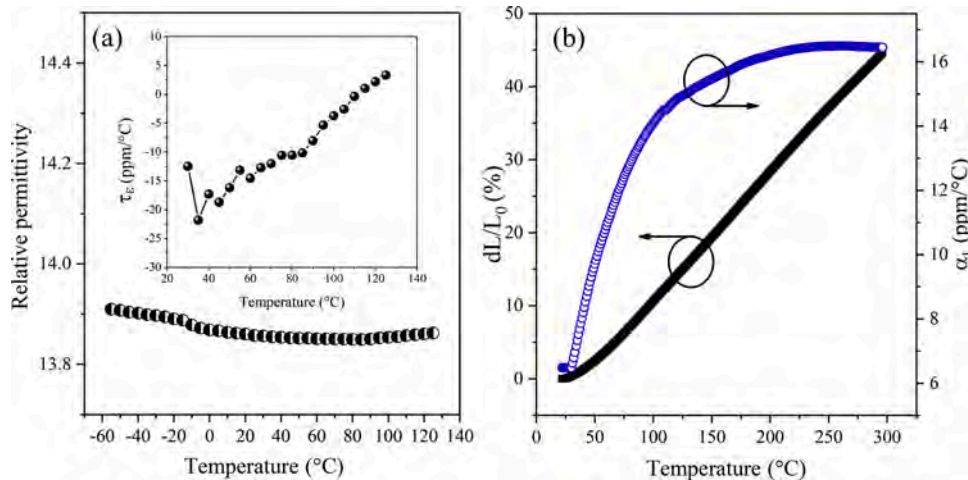
relative permittivity [44]. The former two effects (A and B) are associated with the volume-dependent contribution, and the sum of A and B generally has a small value for oxides, equal to about 6–7 ppm/°C for materials with a permittivity of 15 [44]. The third effect (C) plays a more significant role in  $\tau_\varepsilon$ , related to the temperature dependence of the macroscopic polarizability at constant volume. The macro thermal expansion of ceramic samples is closely correlated to the asymmetric anharmonic vibrations of chemical bonds, directly affected by the binding energy and bond length [45]. Therefore, the near-zero  $\tau_f$  values herein can be ascribed to the small dependence of the polarizability on temperature, moderate asymmetric anharmonic vibrations of chemical bonds, and the opposite signs between  $\alpha_L$  and  $\tau_\varepsilon$  in the temperature range from 25 °C to 85 °C.

Table 1 compares the microwave dielectric properties among some typical compounds with intrinsically low sintering temperatures and low permittivities. As we have mentioned in section 1, near-zero  $\tau_f$  values are scarce among the low-permittivity compounds. Due to its novel temperature stability and relatively low dielectric loss,  $\text{Li}_4\text{MgWO}_6$  shows advantages over the reported dielectrics. To verify the compatibility of the ceramic with Ag electrode, the  $\text{Li}_4\text{MgWO}_6$  green body with Ag coatings was co-fired at 950 °C for 4 h. Fig. S5 shows the cross-section SEM image and EDS line scan of the  $\text{Li}_4\text{MgWO}_6$  ceramic co-fired with Ag electrode. No obvious chemical reaction between the electrode and ceramic matrix was observed, and the EDS line scan spectrum indicated

**Table 1**

Sintering temperature and microwave dielectric properties of some typical compounds with low  $\varepsilon_r$  and low densification temperature.

composition	S.T. (°C)	$\varepsilon_r$	$Q \times f$ (GHz)	$\tau_f$ (ppm/°C)	Ref.
$\text{LiWVO}_6$	700	11.5	13,300	+163.8	[19]
$\text{LiMoVO}_6$	640	13.3	12,500	+101.0	[19]
$\text{Li}_2\text{MoO}_4$	540	5.5	46,000	-160.0	[18]
$\text{Li}_2\text{WO}_4$	650	5.5	62,000	-146.0	[21]
$\text{Li}_2\text{Mg}_2\text{W}_2\text{O}_9$	920	11.5	31,900	-66.0	[22]
$\text{Li}_2\text{Mg}_2(\text{WO}_4)_3$	800	8.2	90,000	-52.4	[23]
$\text{Bi}_2\text{Mo}_3\text{O}_{12}$	610	19.0	21,800	-215.0	[46]
$\text{BaV}_2\text{O}_6$	550	11.2	42,800	+28.2	[47]
$\text{ZnMoO}_4$	850	8.1	48,300	-121.8	[48]
$\text{Li}_6\text{B}_4\text{O}_9$	640	5.95	41,800	-72.0	[49]
$\text{Ba}_2\text{NdV}_3\text{O}_{11}$	880	12.05	23,000	-7.7	[50]
$\text{Ba}_2\text{SmV}_3\text{O}_{11}$	880	12.19	27,100	-16.2	[50]
$\text{Li}_4\text{WO}_5$	890	8.6	23,100	-2.6	[20]
$\text{Li}_4\text{MgWO}_6$	950	15.06 ± 0.33	28,300 ± 600	0.9 ± 3.4	This work



**Fig. 7.** (a) Relative permittivities of the  $\text{Li}_4\text{MgWO}_6$  ceramic sintered at 950 °C for 4 h as a function of temperature (-55 – 125 °C) measured at 1 MHz, the insert image shows the  $\tau_\varepsilon$  values in a wide temperature range ( $t_2 = 30$ –125 °C,  $t_1 = 25$  °C). (b) Thermal expansion ( $dL/L_0$ ) and the thermal expansion coefficient ( $\alpha_L$ ) for the  $\text{Li}_4\text{MgWO}_6$  ceramic sintered at 950 °C for 4 h.



almost no Ag diffusion into the ceramic matrix. With the above advantages,  $\text{Li}_4\text{MgWO}_6$  is a promising low-permittivity candidate material for LTCC applications.

#### 4. Conclusions

In this contribution, a novel  $\text{Li}_4\text{MgWO}_6$  ceramic was synthesized via the conventional solid-state reaction method, and the structural characteristics, sintering behavior, and microwave dielectric properties were studied for the first time. The XRD patterns of the samples taken over a wide temperature range (400–1000 °C) revealed a monoclinic-orthorhombic phase transition for the  $\text{Li}_4\text{MgWO}_6$  ceramic ranging from 800 °C to 900 °C. A tiny amount (wt.% = 1–2 %) of the untransformed monoclinic secondary phase was retained in the orthorhombic main phase for the ceramics sintered above 930 °C. The SAED and HR-TEM photographs taken along the low-index zone axis confirmed the ordered and layered rock-salt superstructures for the orthorhombic  $\text{Li}_4\text{MgWO}_6$  samples. The shrinkage curve showed that the densification of the specimen proceeded in a wide temperature range from 820 °C to 1068 °C, and the SEM photographs and relative density curves indicated the sample had the highest densification at 950 °C. Samples were sintered in a  $\text{WO}_3$ -rich atmosphere provided by a designed device to prevent  $\text{WO}_3$  from subliming at the sintering range. The sample sintered at 950 °C for 4 h showed a high relative density of 95.66 % and a high packing fraction of 72.7 %. The optimum microwave dielectric properties were obtained with  $\epsilon_r = 15.06 \pm 0.33$ ,  $Q \times f = 28,300 \pm 600$  GHz ( $f = 10.1$  GHz), and  $\tau_f = 0.9 \pm 3.4$  ppm/°C. Due to its intrinsic low sintering temperature, novel temperature stability, relatively low dielectric loss, and good chemical compatibility with Ag electrodes,  $\text{Li}_4\text{MgWO}_6$  is a promising material for LTCC applications.

#### Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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#### Appendix A. Supplementary data

Supplementary material related to this article can be found, in the online version, at doi:<https://doi.org/10.1016/j.jeurceramsoc.2021.09.010>.

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